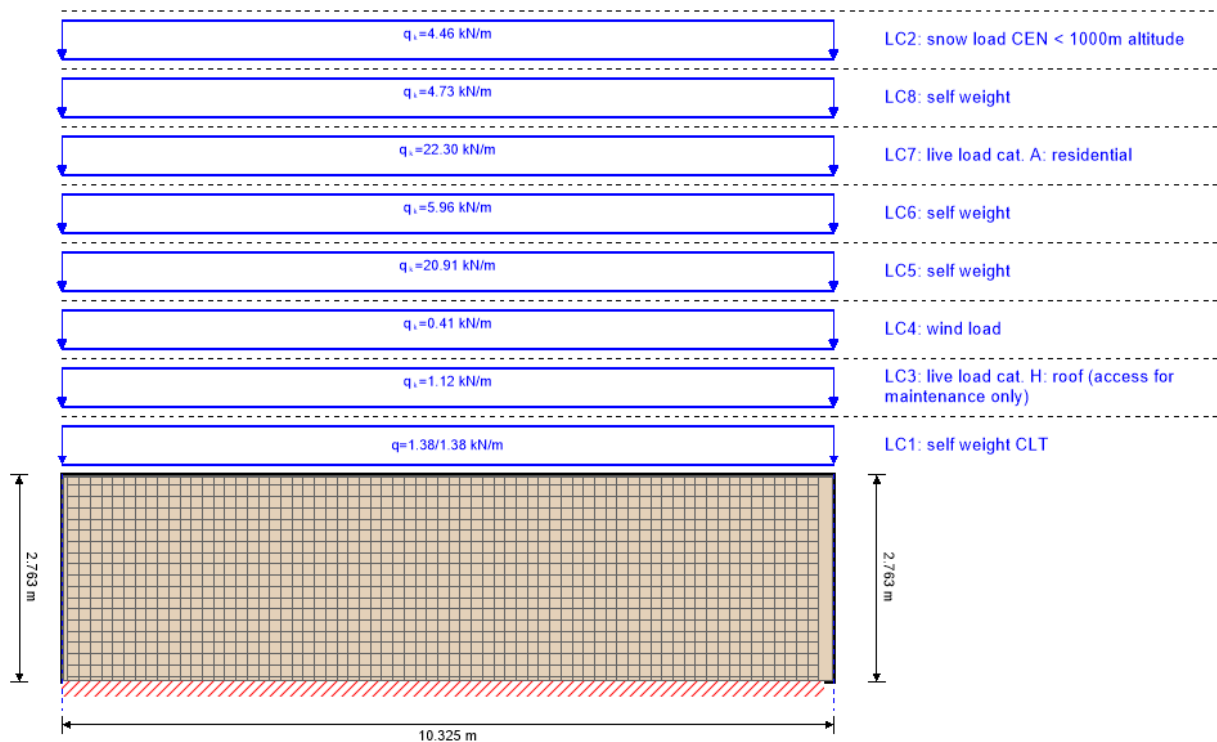


system

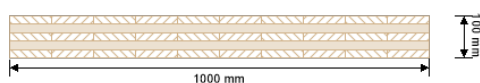


global utilization ratio

25 %

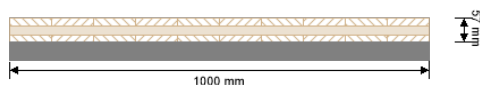
ULS	22 %	ULS fire	25 %	SLS	0 %
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section: CLT 100 L5s



layer	thickness	orientation	material
1	20.0 mm	0°	C24 spruce ETA (2019)
2	20.0 mm	90°	C24 spruce ETA (2019)
3	20.0 mm	0°	C24 spruce ETA (2019)
4	20.0 mm	90°	C24 spruce ETA (2019)
5	20.0 mm	0°	C24 spruce ETA (2019)
t _{CLT}	100.0 mm		

section fire: CLT 100 L5s



layer	thickness	orientation	material
1	20.0 mm	0°	C24 spruce ETA (2019)
2	20.0 mm	90°	C24 spruce ETA (2019)
3	17.0 mm	0°	C24 spruce ETA (2019)
t _{CLT}	57.0 mm		
fire resistance class: R 90	time	90 min	

section fire: CLT 100 L5s

fire protection layering : 2 x 12.5 mm gypsum plasterboard
Type F
gypsum plasterboard Type A (acc. to EN 520)gypsum plasterboard
Type F (acc. to EN 520)

$t_{ch,h}$	$t_{f,h}$	$t_{a,h}$	$d_{ta,h}$	k_0	d_0	$d_{char,0,h}$	$d_{ef,h}$
[min]	[min]	[min]	[mm]	[-]	[mm]	[mm]	[mm]
49	54	72	25	1	7	37.0	44.0

material values

material	$f_{m,k}$	$f_{t,0,k}$	$f_{t,90,k}$	$f_{c,0,k}$	$f_{c,90,k}$	$f_{v,k}$	$f_{r,k \text{ min}}$	$E_{0,mean}$	G_{mean}	$G_{r,mean}$
	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[N/mm ²]
C24 spruce ETA (2019) C24 spruce ETA (2019)	24.00	14.00	0.12	21.00	2.50	4.00	1.25	12,000.00	690.00	50.00

load
load case groups

	load case category	Typ	duration	Kmod	γ_{inf}	γ_{sup}	ψ_0	ψ_1	ψ_2
LC1	self weight CLT	G	permanent	0.6	1	1.35	1	1	1
LC1	self weight CLT	G	permanent						
LC2	snow load CEN < 1000m altitude	Q	short term	0.9	0	1.5	0.5	0.2	0
LC2	snow load CEN < 1000m altitude	Q	short term						
LC3	live load cat. H: roof (access for maintenance only)	Q	short term	0.9	0	1.5	0	0	0
LC3	live load cat. H: roof (access for maintenance only)	Q	short term						
LC4	wind load	Q	short term	0.9	0	1.5	0.6	0.2	0
LC4	wind load	Q	short term						
LC5	self weight	G	permanent	0.6	1	1.35	1	1	1
LC5	self weight	G	permanent						
LC6	self weight	G	permanent	0.6	1	1.35	1	1	1
LC6	self weight	G	permanent						
LC7	live load cat. A: residential	Q	medium term	0.8	0	1.5	0.7	0.5	0.3
LC7	live load cat. A: residential	Q	medium term						
LC8	self weight	G	permanent	0.6	1	1.35	1	1	1
LC8	self weight	G	permanent						

LC1:self weight CLT

trapezoidal load			
distance from start	$q_{k,a}$	load at end	load length
[m]	[kN/m]		[m]
0.000	1.3815	1.38	10.325

LC2:snow load CEN < 1000m altitude

continuous load	
q_k	
[kN/m]	
4.46	

LC3:live load cat. H: roof (access for maintenance only)

continuous load	
q_k	
[kN/m]	
1.115	

LC4:wind load

continuous load

q_k

[kN/m]

0.41

LC5:self weight

continuous load

q_k

[kN/m]

20.91

LC6:self weight

continuous load

q_k

[kN/m]

5.957

LC7:live load cat. A: residential

continuous load

q_k

[kN/m]

22.3

LC8:self weight

continuous load

q_k

[kN/m]

4.7319

ULS combinations

	combination rule
LCO1	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8$
LCO1	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8$
LCO2	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2$
LCO2	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2$
LCO3	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2 + 1.50/0.00 * 0.00 * LC3$
LCO3	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2 + 1.50/0.00 * 0.00 * LC3$
LCO4	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2 + 1.50/0.00 * 0.00 * LC3 + 1.50/0.00 * 0.60 * LC4$
LCO4	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2 + 1.50/0.00 * 0.00 * LC3 + 1.50/0.00 * 0.60 * LC4$
LCO5	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2 + 1.50/0.00 * 0.00 * LC3 + 1.50/0.00 * 0.60 * LC4 + 1.50/0.00 * 0.70 * LC7$
LCO5	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC2 + 1.50/0.00 * 0.00 * LC3 + 1.50/0.00 * 0.60 * LC4 + 1.50/0.00 * 0.70 * LC7$
LCO6	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC3$
LCO6	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC3$
LCO7	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC3 + 1.50/0.00 * 0.50 * LC2$
LCO7	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC3 + 1.50/0.00 * 0.50 * LC2$
LCO8	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC3 + 1.50/0.00 * 0.50 * LC2 + 1.50/0.00 * 0.60 * LC4$
LCO8	$1.35/1.00 * LC1 + 1.35/1.00 * LC5 + 1.35/1.00 * LC6 + 1.35/1.00 * LC8 + 1.50/0.00 * LC3 + 1.50/0.00 * 0.50 * LC2 + 1.50/0.00 * 0.60 * LC4$

[illegible][illegible]

ULS combinations fire	
	combination rule
LCO13 LCO13	1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.00 * LC4 + 1.00/0.00 * 0.00 * LC2 + 1.00/0.00 * 0.00 * LC3 + 1.00/0.00 * 0.30 * LC7 1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.00 * LC4 + 1.00/0.00 * 0.00 * LC2 + 1.00/0.00 * 0.00 * LC3 + 1.00/0.00 * 0.30 * LC7
LCO14 LCO14	1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7
LCO15 LCO15	1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 + 1.00/0.00 * 0.00 * LC2 1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 + 1.00/0.00 * 0.00 * LC2
LCO16 LCO16	1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 + 1.00/0.00 * 0.00 * LC2 + 1.00/0.00 * 0.00 * LC3 1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 + 1.00/0.00 * 0.00 * LC2 + 1.00/0.00 * 0.00 * LC3
LCO17 LCO17	1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 + 1.00/0.00 * 0.00 * LC2 + 1.00/0.00 * 0.00 * LC3 + 1.00/0.00 * 0.00 * LC4 1.00/1.00 * LC1 + 1.00/1.00 * LC5 + 1.00/1.00 * LC6 + 1.00/1.00 * LC8 + 1.00/0.00 * 0.30 * LC7 + 1.00/0.00 * 0.00 * LC2 + 1.00/0.00 * 0.00 * LC3 + 1.00/0.00 * 0.00 * LC4

Ultimate limit state (ULS) - design results

utilization rate of shear stress in plane on net section

0.0 %
0.0 %

100.0 %

LCO14

Id	X	Z	k _{mod}	f _{IP,Netto,k}	Q	T _{IP,Net,d}	ratio
[-]	[m]	[m]	[-]	[N/mm²]	[kN]	[N/mm²]	[%]
1182	3.825	2.475	0.8	3.9	0.00	0.00	0 %

utilization rate of shear stress in plane of gross section

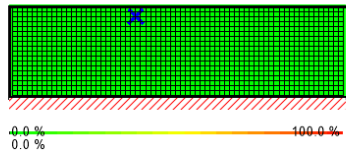
0.0 %
0.0 %

100.0 %

LCO14

Id	X	Z	k _{mod}	f _{v,IP,Brutto,k}	Q	τ _{IP,Gross,d}	ratio
[-]	[m]	[m]	[-]	[N/mm²]	[kN]	[N/mm²]	[%]
1182	3.825	2.475	0.8	3.5	0.00	0.00	0 %

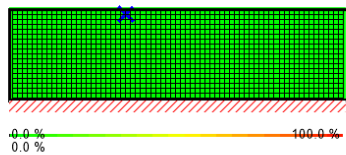
utilization rate of torsional shear stress in face glued surfaces



LCO14

Id	X	Z	k_{mod}	$f_{v,IP,T,k}$	Q	$T_{T,Node,d}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[N/mm ²]	[%]
1182	3.825	2.475	0.8	2.5	0.00	0.00	0 %

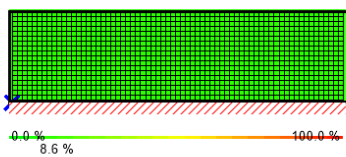
utilization rate of axial force horizontal



LCO14

Id	X	Z	k_{mod}	$f_{m,k}$	$N_{h,max}$	M_y	$\sigma_{h,max}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[kNm]	[N/mm ²]	[%]
1248	3.525	2.625	0.8	24.0	0.0000	0.0000	0.00	0 %

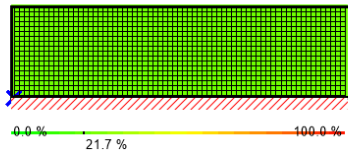
utilization rate of axial force vertical



LCO14

Id	X	Z	k_{mod}	$f_{m,k}$	$N_{v,max}$	M_y	$\sigma_{v,max}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[kNm]	[N/mm ²]	[%]
1	0.075	0	0.8	24.0	1.8394	0.0000	1.32	9 %

utilization rate for buckling

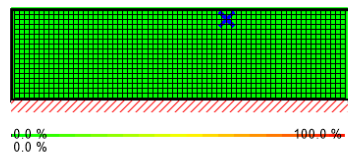


LCO14

Id	X	Z	I_k	λ_y	β_c	$k_{c,y}$	$f_{c,d}$	$\sigma_{c,0,d}$	$\sigma_{m,y,d}$	ratio
[-]	[m]	[m]	[m]	[-]	[-]	[-]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[%]
1	0.075	0	2.763	83	0.2	0.45	13.44	1.32	0.00	22 %

Ultimate limit state (ULS) fire design - results

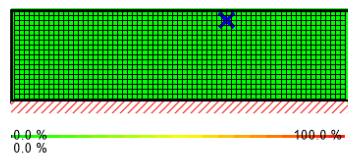
utilization rate of shear stress in plane on net section



LCO5

Id	X	Z	k_{mod}	$f_{IP,Netto,k}$	Q	$T_{IP,Net,d}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[N/mm ²]	[%]
1200	6.525	2.475	1	3.9	0.00	0.00	0 %

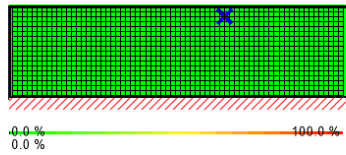
utilization rate of shear stress in plane of gross section



LCO5

Id	X	Z	k_{mod}	$f_{v,IP,Brutto,k}$	Q	$\tau_{IP,Gross,d}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[N/mm ²]	[%]
1200	6.525	2.475	1	3.5	0.00	0.00	0 %

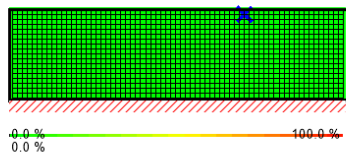
utilization rate of torsional shear stress in face glued surfaces



LC05

Id	X	Z	k_{mod}	$f_{v,IP,T,k}$	Q	$T_{T,Node,d}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[N/mm ²]	[%]
1200	6.525	2.475	1	2.5	0.00	0.00	0 %

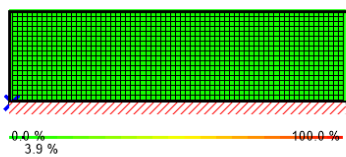
utilization rate of axial force horizontal



LC05

Id	X	Z	k_{mod}	$f_{m,k}$	$N_{h,max}$	M_y	$\sigma_{h,max}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[kNm]	[N/mm ²]	[%]
1272	7.125	2.625	1	24.0	0.0000	0.0000	0.00	0 %

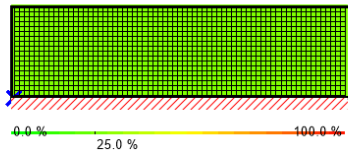
utilization rate of axial force vertical



LC05

Id	X	Z	k_{mod}	$f_{m,k}$	$N_{v,max}$	M_y	$\sigma_{v,max}$	ratio
[-]	[m]	[m]	[-]	[N/mm ²]	[kN]	[kNm]	[N/mm ²]	[%]
1	0.075	0	1	24.0	6.0235	0.0000	1.09	4 %

utilization rate for buckling

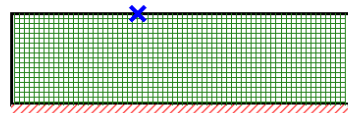


LC05

Id	X	Z	I_k	λ_y	β_c	$k_{c,y}$	$f_{c,d}$	$\sigma_{c,0,d}$	$\sigma_{m,y,d}$	ratio
[-]	[m]	[m]	[m]	[-]	[-]	[-]	[N/mm ²]	[N/mm ²]	[N/mm ²]	[%]
1	0.075	0	2.763	139	0.2	0.18	24.15	1.09	0.00	25 %

Service limit state design (SLS) - design results

horizontal deformation



LC05

Id	X	Z	W_{limit}	limit	$V_{h,max}$	ratio
[-]	[m]	[m]	[mm]	[mm]	[mm]	[%]
1386	3.825	2.763	9.2	$L/300 = 9.2$ $L/300 = 9.2$	0.0000	0.0 %

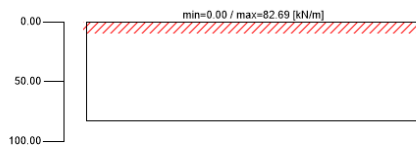
support reaction

support reaction horizontal min/max

min=0.00 / max=0.00 [kN/m]



support reaction vertical min/max



support reaction moment min/max

min=0.00 / max=0.00 [kNm/m]



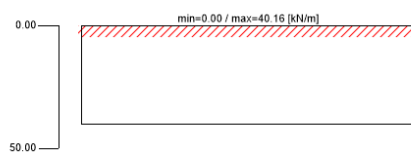
fire support reaction

fire support reaction horizontal min/max

min=0.00 / max=0.00 [kN/m]



fire support reaction vertical min/max



fire support reaction moment min/max

min=0.00 / max=0.00 [kNm/m]



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